

# A Review of Voltage Distribution on Metal Oxide Surge Arrester and Suggestions for Improvement in High Voltage Applications

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**Abstract**—Stray capacitive effect of Metal Oxide Surge Arrester (MOSA) may cause non-uniform voltage distribution in both non-conduction and conduction modes. Also, during conduction, there is a delay in operation of arrester, particularly when faced with very fast transient overvoltages (VFTOs). Consequently, there is a necessity to reduce stray capacitive effect for improvement in voltage distribution and reduce delay in response of arrester for VFTOs. One approach is placement of grading rings with appropriate number and size. Numerous researchers have conducted extensive studies on causes of non-uniform voltage distribution, computation of stray capacitances and remedial measures to achieve a more uniform voltage distribution. Further, this investigation holds great significance in polluted environments, damaged arresters and broken sheds, as proper operation of surge arresters relies on environmental conditions, material properties, and shapes of arrester assembly. This paper provides a summary of research conducted by various researchers from the year 1970 and also offers suggestions for further studies of achieving a more uniform voltage distribution and reducing response delay of MOSAs.

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**Index Terms**—Block capacitance, Conduction mode, Metal oxide surge arrester (MOSA), Non-conduction mode, Very fast transient overvoltage (VFTO), Stray Capacitance.

## I. INTRODUCTION

METAL oxide surge arresters (MOSAs) are composition of various chemicals like zinc oxide, bismuth oxide, cadmium oxide, boron oxide, praseodymium oxide, aluminum oxide and silicon oxide [1], [2]. Zinc oxide remains as dominant element in this composition, accounting for approximately 95-97% of entire resistor with smaller amounts of other metal oxides [3], [4] for controlling non-linearity within the resistor [5] - [11]. The molded arrester blocks are typically stacked within porcelain or polymeric insulators. An equal voltage is to be applied across each block and hence, a linear axial voltage gradient distribution is expected. But, there is a deviation from linear nature because of stray (inherent) capacitance. Since, it varies with height of arrester, the deviation from linear nature is increased with its height, making design of MOSAs as cumbersome [12] - [33]. This stray capacitance (SC) makes non-uniformity of voltage distribution

[34] - [36] and is reduced by placing of grading rings with new arrester materials [37] - [44]. This paper summarizes voltage distribution study made on MOSA by different researchers from the year 1970 to till date with a case study.

## II. DIMENSION OF SINGLE STACK ARRESTER

The arrester blocks are housed in a hermetically sealed hollow porcelain insulator [30]. Fig. 1 shows arrester blocks and dimension of a single stack (66 kV) arrester.

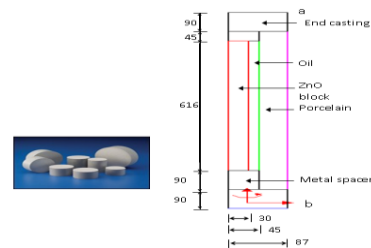


Fig. 1. Arrester blocks and Dimensional details of single stack arrester (mm).

## III. STRAY CAPACITANCE

It is a capacitive effect between any high voltage point and ground. This is more significant in high voltage MOSAs and is very difficult to measure. In early years, researchers have used approximate empirical formulae for finding stray capacitance by assuming basic electrode shapes [14]. The accurate dimensions are not incorporated in empirical formulae and also for adding grading ring effects, Finite Element Method (FEM) is used for calculating arrester stray capacitance [13], [15], [17], [45], [46]. Electric field around MOSA in both clean and polluted arresters with varying fibre glass thickness and electrodes height sheds are computed [47].

## IV. ILL-EFFECTS OF ARRESTER STRAY CAPACITANCE

The behavior of MOSA depends on distributed stray capacitive effect during both steady state and transient conditions. In non-conduction mode (power frequency voltage), upper portion of blocks are subjected to higher potential gradient since supply voltage is appeared continuously across MOSA. So, higher thermal stresses occur, lead to faster thermal ageing across these stressed blocks with less lifetime [25], [28], [42] - [52]. The voltage non-uniformity during conduction mode (high frequency transient operation) is also more significant with increased steepness of applied current surge [30]. Hence, MOSA behaves as capacitor and inoperative under transients of nanosecond ranges, especially in SF<sub>6</sub> based substation with high voltage rating.

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V. VOLTAGE DISTRIBUTION UNDER NON-CONDUCTION MODE

Since leakage current due to resistance is very small, distribution of voltage is calculated only based on arrester capacitances [17], [18], [53]. There are various service conditions like elevated installation, provision of nearby energized apparatus and earthed objects, which may also influence voltage distribution [12]. The key points for this section is summarized in Table I.

TABLE I  
SUMMARIZED KEY POINTS FOR VOLTAGE DISTRIBUTION

Methods	Findings	Ref
Analytical approach and wireless current	Potential distribution in all conditions	[47], [54], [55]
Electrical field and circuit	Analyzing distribution of potential in arresters	[56]
FEM based analytical method	Solving open boundary axisymmetric electrostatic problems	[57]
FEM based analytical method	3D based potential distribution	[58]
3D FEM and circuit analysis	Potential distribution on 1000 kV gas insulated MOSA	[59]
3D FEM	Comparison of gas insulated MOSAs	[60]
3D FEM	Distribution of potential and stray capacitances	[61]-[64].
FEM	Grading ring optimization	[65]-[67]
Maxwell and EMTP/ATP software	Electric field and leakage current	[68]
FEM	Electric field distribution and optimized grading ring	[69]

Three dimensional design may be used to change geometry or materials for achieving good performance values [25], [26]. There is existing of stray capacitances with high value in SF<sub>6</sub> based MOSA because of earthed metal housing [70], [71]. Here, an attempt is made to compute stray capacitance, Voltage Distribution (VD) for non-conduction and conduction modes and delay in response of arrester for 198 kV arrester as case study. Different arrester ratings, 66 kV (single stack:1×66 kV) to 396 kV (six stacks:6×66 kV) are taken for computing stray capacitance and distribution of voltage.

VI. STRAY CAPACITANCE AND DISTRIBUTION OF VOLTAGE FOR VARIOUS HEIGHTS OF MOSA

The stray capacitance and distribution of voltage for different heights are computed using FEM. Table II gives stray capacitance. The voltage in per unit (pu) for single stack (66kV), three stack (198kV) and six stack (396kV) are plotted (Fig.2). There is an increase in non-uniformity of voltage distribution for higher arrester heights. Comparing single stack, six stack arrester is having more non-uniformity.

A. Remedial Measures – Grading rings

Even though many corrective measures are available, one of the methods, generally used for improving voltage non-uniformity is placing of grading rings [72], [73].

TABLE II  
STRAY CAPACITANCE - DIFFERENT HEIGHTS OF MOSA

kV	Ht (mm)	SC (pF)
66	2116	2.1
132	2732	4.58
198	3348	6.78
264	3964	8.86
330	4580	10.78
396	5196	14.61

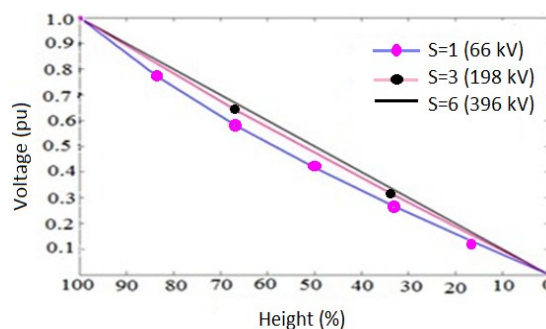


Fig. 2. Voltage Distribution -Various heights (S: no. of stacks).

B. Other Remedial Measures

Internal grading circuit, capacitive or resistive elements are employed [15], [17], [18]. This is achieved by placing higher capacitance block at upper portion of arrester and lower capacitance block at bottom portion of arrester. The distribution of voltage is made more uniform on arresters using spacers and Fiberglass Reinforce Plastic (FRP) layers by proper geometries, materials and different surrounding insulation materials [49]. The parallel capacitors are considered to achieve potential distribution coefficient within ±15% [21], [74], [59], but recommended value is less than 5% [61], [62].

C. Case Study for Non-conduction Mode -198kV arrester

An arrester having three stacks with two grading rings, Fig. 3 (a), location of grading rings, Fig. 3 (b) and voltage distribution during non-conduction mode, Fig. 3 (c) are shown. The results are validated with reference [75].

VII. VOLTAGE DISTRIBUTION UNDER POLLUTED ENVIRONMENT AND BROKEN SHEDS

Non-uniform electric field distribution exists in polluted environmental conditions. The geometry, electrical properties of various components and location of broken shed influence voltage distribution on MOSA [76] - [78]. The arrester housing becomes conducting when it is polluted and redistributes voltage distribution. Generally, resistance of external portion of arrester in clean environmental condition is very high. But, in contaminated conditions, external part of arrester gains some conductivity and hence its resistance decreases. Because of these variations of resistance inside and outside the arrester, distribution of voltage becomes uneven. The arrester blocks undergo an enormous heating resulting as thermal runaway phenomenon. As a consequence, destruction of complete arrester assembly happens. So, successful operation depends on environments. But, mis-operation of arrester on housing is due

to dirt or ash from industries, sea salt and sand accumulation. A suggestion is given for revision of ANSI Standard for demonstrating ability of arresters to permit washing while energized [25], [79] - [83].

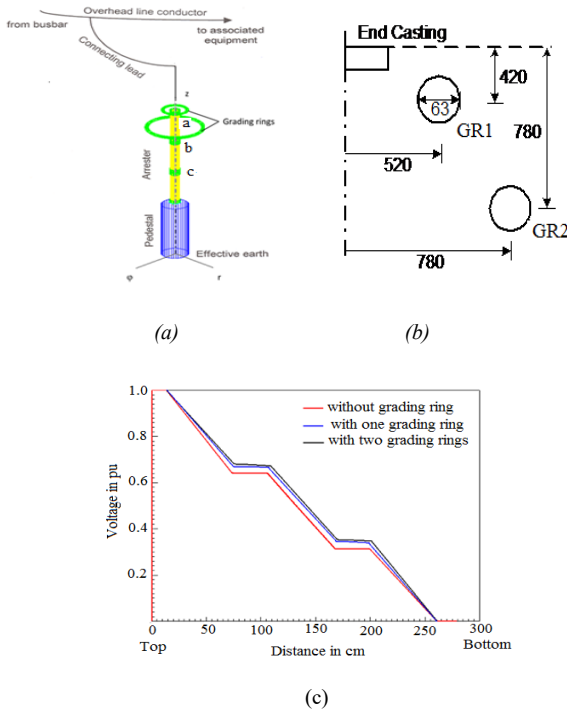


Fig. 3. 3-stack MOSA: (a) Position of grading rings, (b) Dimensions of grading ring in mm, (c) Voltage distribution.

VIII. VOLTAGE DISTRIBUTION DURING CONDUCTION MODE

The effect of capacitance during transient mode of arrester is analyzed by computing discharge voltage of arrester with different current surges. The stray capacitance gives considerable effect during nanosecond surges [23]. The electrical stress across upper-most stack of arrester is more during nanoseconds. This stress is increased with higher height or voltage rating of arrester as well as applied current surge with less front time. The increased stress may be reduced by placing suitable number of grading rings in suitable locations. Moreover, arrester with higher gradient material may also reduce height of arrester and hence stray capacitance is reduced. MCOV of arrester:181kV<sub>rms</sub>, discharge voltage: 600kV, discharge current:10kA, non-linear index :50.

A. Case Study for Conduction Mode - 198kV Arrester

The voltages at various stacks / metal flanges (a, b, c) are simulated with accurately computed stray capacitance for two different current surges as shown in Fig. 4 (a) and Fig. 4(b). There is a non-uniformity in distribution of voltage, which increases for applied current surges with less front time, Fig 4. (b) and is reduced with grading rings in suitable positions.

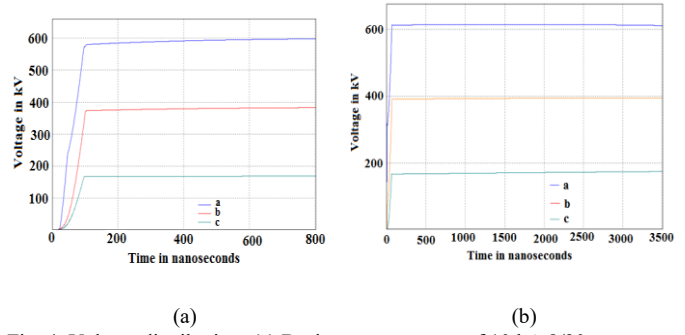


Fig. 4. Voltage distribution: (a) During current surge of 10 kA,8/20 μs, (b) During current surge of 10 kA,5ns/10 μs ( a, b, c: metal flanges).

When arrester is conducting successfully, its discharge voltage peaks before peak value of applied current surge, shown in Fig.5 (a). When front time of applied current surge is decreased, especially for nanosecond surges, its discharge voltage peaks after occurrence peak of applied current surge, given in Fig. 5 (b). This is because of presence of delay (time lag) in response of arrester. This delay must be reduced for successful conduction of MOSA.

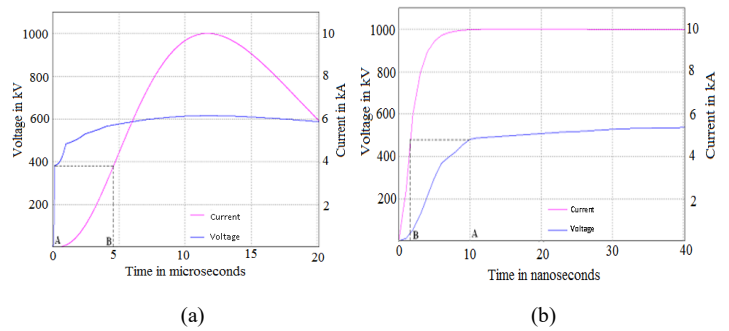


Fig. 5. Showing delay in response: (a) Conduction of 10 kA,8/20μs current surge, (b) Conduction of 10 kA,5ns/10μs current surge.

B. Placing of Grading Rings

Using details of grading rings, obtained from manufacturer, simulation is carried out for different applied current surges. The voltage appeared across topmost stack is given in Table III.

TABLE III  
VOLTAGE ACROSS TOP STACK IN KV

1μs/10μs	5ns/10μs	5ns/10μs (with grading rings)
215.0	219.2	213.8

It is found that, before placing grading rings, when steepness of applied current surge is increased from 1 μs to 5 ns, voltage across top stack is increased from 215.0 kV to 219.2 kV. After placing two grading rings, voltage is reduced from 219.2 kV to 213.8 kV. Even though reduction in non-uniformity is there, this may not be sufficient for successful operation, especially for higher voltage ratings of arrester. Hence another alternative measure is chosen, like addition of new materials.

IX. NEW COMPOSITION OF MATERIAL

The voltage of about twice that of conventional arrester for rating from 66 kV up to 500 kV with reduced height is obtained

by decreasing average grain size of ZnO with a newly added material and improved process of sintering [84] - [90]. The usage of these higher gradient arresters may give flexibility while locating MOSAs in SF<sub>6</sub> based substations [91]- [94]. The conventional arrester elements have lower reference voltage of 200 Volts/mm and could be further increased by 1.5 to 2 times with development of high voltage gradient of 300 Volts/mm [95]. The high voltage gradient (435Volts/mm) arresters could improve distribution of potential along arrester columns by 10% [95] - [97]. The rare earth oxides slow down grain growth because of stabilization of new spinel phases achieved at grain boundary. A uniform high voltage gradient of 600 Volts/mm is developed by controlling grain growth of ZnO with modified process of manufacturing. Doping with rare earth would significantly improve electrical behavior of ZnO arrester blocks like nonlinear coefficient, voltage gradient, and leakage current. The effects of Co<sub>2</sub>O<sub>3</sub> on phase composition, electrical behavior, micromorphology and dielectric properties of ZnO blocks are presented [98] - [100]. Hence, leakage current reduction, grain resistivity enhancement and non-linear coefficient improvement in Co-doped ZnO arrester blocks are understood. Finally, there is reduction of grain size, height and compactness of arrester with improvement of distribution of voltage in both steady and transient states of power system [39], [101] - [103].

#### X. SHORTENING OF ARRESTER COLUMNS USING HIGH GRADIENT MATERIAL – SCANDIUM OXIDE

The operational time delay between arrester discharge voltage and current is minimized by reducing arrester capacitive effect with reduction of height of arrester column. The ZnO (MOSA) arrester with high voltage gradient material plus Rare Earth (RE) additives shortens length of arrester and also RE elements bring better results when used with ZnO-Bi<sub>2</sub>O<sub>3</sub> based arrester materials. A few selected RE additives like Sc<sub>2</sub>O<sub>3</sub>, Yb<sub>2</sub>O<sub>3</sub>, Y<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub> and Dy<sub>2</sub>O<sub>3</sub> have features to improve arrester performance. Among them, Sc<sub>2</sub>O<sub>3</sub> is found to be the best suited to effect the required higher arrester voltage gradient. On mixing it with other arrester basic ingredients, a better control over grain growth during sintering process is established. This control is considered as a factor to bring a strong pinning effect and reduced grain sizes. Further, addition of Sc<sub>2</sub>O<sub>3</sub> enhances grain boundaries and increases possibility of getting material of better potential gradient for blocks of MOSA. The blocks of surge arrester are prepared with reagent raw materials, ZnO in major proportion and a small quantum of Bismuth (III) Oxide, Antimony (III) Oxide, Cobalt (III) Oxide, Chromium (III) Oxide, Manganese dioxide, and Scandium (III) Oxide. The required weighed powders are put in a nylon jar having zirconia balls. Ball milling method is carried out with a wetting agent. The ratio of powder to balls is taken as 1:10. This process is done for ten hours. For two hours, the taken powders are heated at 600°C. Using Agate/mortar, the heated powders are pulverized after adding 2wt% of Poly Vinyl Alcohol. Then the powders are crystallized into grains by sieving through a 100 mesh screen. Now, in a die, the prepared powder is placed and then in a uniaxial pressing machine. Afterwards, this is pressed. A pressure of 150Mpa is applied for making the powders in to discs. A density of about 55% of its theoretical density is found

for wet / green cylindrical arrester. Now the arrester disc is ready for process of sintering. The arrester sample is subjected to various required processes of sintering. Finally, required dimensions of arrester samples are obtained after employing lapping and grinding machines. Now the entire process is completed for making an arrester block. The resultant block takes the shape of an innovative new composition arrester blocks. For conventional arrester disc, voltage gradient is in the range of 475-520Volts/mm and method currently in practice brings non-uniform heating effect. Moreover, there are higher height of arrester columns and more capacitance effect. Hence, performance under all types of VFTOs are not at the desired level. For genetically modified ZnO arrester disc (addition of RE viz., Sc<sub>2</sub>O<sub>3</sub>), voltage gradient is to achieve higher voltage gradient of maximum value of 825Volts/mm. Microwave sintering produces uniform heating with the attendant higher densification of arrester discs by reduced holding duration for the disc, which brings higher breakdown fields. The height of arrester is low and hence performance under all types of VFTOs are exceedingly good. The microstructures of conventional and new composition arresters reveal that there is a lower value in grain sizes, a higher value in voltage gradients and reduced height requirement per unit for genetically modified arresters. Consequently, the newly developed ZnO surge arrester with high-gradient materials enhances its behavior and improves voltage distribution by mitigating stray capacitance effect through reduced height.

#### XI. FUTURE RESEARCH

Finite element methods and intelligent techniques are used for computing stray capacitance and voltage distribution of arresters. The stray capacitance is increased with height of MOSA column, but its reduction is achieved with new dimensions of grading rings and different composition of materials with suitable manufacturing process. Rare earth elements are very suitable for obtaining required higher voltage gradient arrester. Scandium Oxide is one among them, which enhances grain boundaries and increase possibility of formation of improved value of voltage gradient material for arrester, hence there is a reduction of length or height of arrester. The distribution of voltage across SF<sub>6</sub> based MOSA is more uniform as compared to conventional MOSAs because of increased stray capacitances resulted from grounded metallic enclosure. Gas insulated arrester of ratings, above 245kV are in practice and hence, further studies on these arresters are very much essential in future with good design of grading rings. Also as future work, it is suggested that new materials, like Scandium Oxide may be used for further reduction of height of arrester. So, fabrication of genetically modified MOSAs (modified ZnO arrester) with innovative fabrication techniques and sintering process may help in bringing an effective MOSA under all VFTOs.

#### XII. CONCLUSIONS

This paper discusses an extensive review made on voltage distribution of arresters from the year 1970 (5+ decades). Researchers have found that there is non-uniformity of distribution of voltage along height of arresters during their steady and transient states of operation due to stray capacitance.

Few remedial measures, like placing grading rings and connecting series capacitors, have been described to make voltage distribution more uniform. A case study is used to compute capacitance and distribution of voltage using FEM. There is a reduction of non-uniformity of voltage distribution after placing grading rings. The suggested measures may not be sufficient to make required uniformity since voltage level of power systems are increasing day by day. Finally, it is observed from reported work and case study that non-uniformity of voltage distribution decreases significantly with reducing height of arrester, which is achieved with material of higher voltage gradient. In future, preparation of new high gradient arrester material would be a suitable method for achieving reduced height of arrester with excellent non-linear as well as electrical characteristics. The same voltage distribution study may be carried out in polluted environments, damaged arresters and broken sheds. The modifications in arrester are having effect under both steady and transient states of operation.

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